

# Thermal and Electrical Performance Evaluation and Design Optimization of Hybrid PV/T Systems

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## Abstract

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This study aims to evaluate the performance and cooling effectiveness of both photovoltaic (PV) and hybrid PV/thermal systems under various ambient conditions. Two models, namely standard PV module subject to ambient conditions without active cooling and a single-pass hybrid PV/T air collector, have been designed and simulated using the CFD software of COMSOL Multiphysics V5.3a. The PV material used in our analysis is monocrystalline silicon with a power temperature coefficient of  $0.41\% \text{ } ^\circ\text{C}^{-1}$ . The thermal and electrical performances of both systems are evaluated numerically and compared to experimental data for validation. The results predicted for cooling effects show noticeable enhancements in both the electrical and thermal efficiencies of the systems, with up to 44% compared to the PV module without active cooling. The electrical PV/T arrangement has increased the performance of air cooling in a laminar flow regime with up to 4%. A numerical-based design optimization is carried out to enhance the system performance.

## Keywords

Conjugate heat transfer  
Cooling enhancement  
Design optimization  
Hybrid efficiency  
Hybrid PV/T  
Photovoltaic

## 1. Introduction

Photovoltaic (PV) systems have witnessed exceptional development in the last two decades where it has been shown that a PV panel can absorb more than 75% of the insolation. Only a limited percentage of light waves, however, can be transformed into electricity (10–18%), with the rest wasted as heat into the cells, thus increasing the PV temperature dramatically. As a result, the cell efficiency is predicted to drop by 0.4–0.65% for each  $1 \text{ } ^\circ\text{C}$ , when the temperature is above standard conditions ( $25 \text{ } ^\circ\text{C}$  and  $1000 \text{ W m}^{-2}$ ) [1, 2]. Therefore, it is important to establish a mechanism to address these issues. A hybrid solar energy system known as photovoltaic/thermal (PV/T) utilizes the features of thermal and solar means to produce thermal and electrical energies simultaneously. The exploitation of the hybrid photovoltaic/thermal (PV/T) technology aims to tackle this problem by keeping the PV cell temperature in its optimal range, which in turn improves the efficiency and produces heat and electricity simultaneously.

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In order to improve efficiency of PV/T air collector, several attempts have been made to examine the effects of

extended surfaces on improving the overall (hybrid) efficiency of a PV/T air system. Extended surfaces can be classified into three main categories: (1) traditional fins [3, 4, 5], (2) interposition of a thin metallic sheet [6, 7, 8, 9] (TMS), and (3) obstacles or ribs [10, 11, 12, 13]. Little attention however has been paid to study the impact of offset strip fins within PV/T air systems using optimization strategy [14, 15, 16]. This study is aimed to evaluate the performance of a PV module, without active cooling (i.e. PV module is subject to ambient conditions) and with active cooling a single-duct single-pass hybrid PV/T air collector.

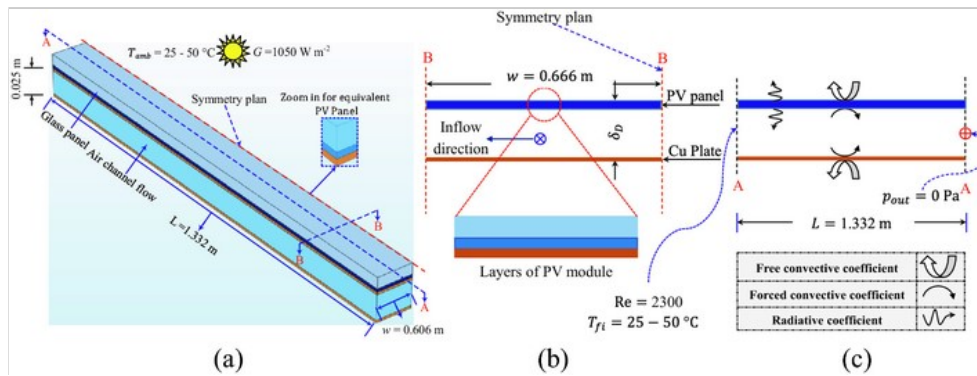
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## 2. Numerical Investigation

Three-dimensional models of single-pass PV/T solar air designs and a PV module have been constructed using the COMSOL Multiphysics V5.3a CFD modelling software. All dimensions of the two systems are listed in Tables 1 and 2, and schematics are provided in Figs. 1 and 2.

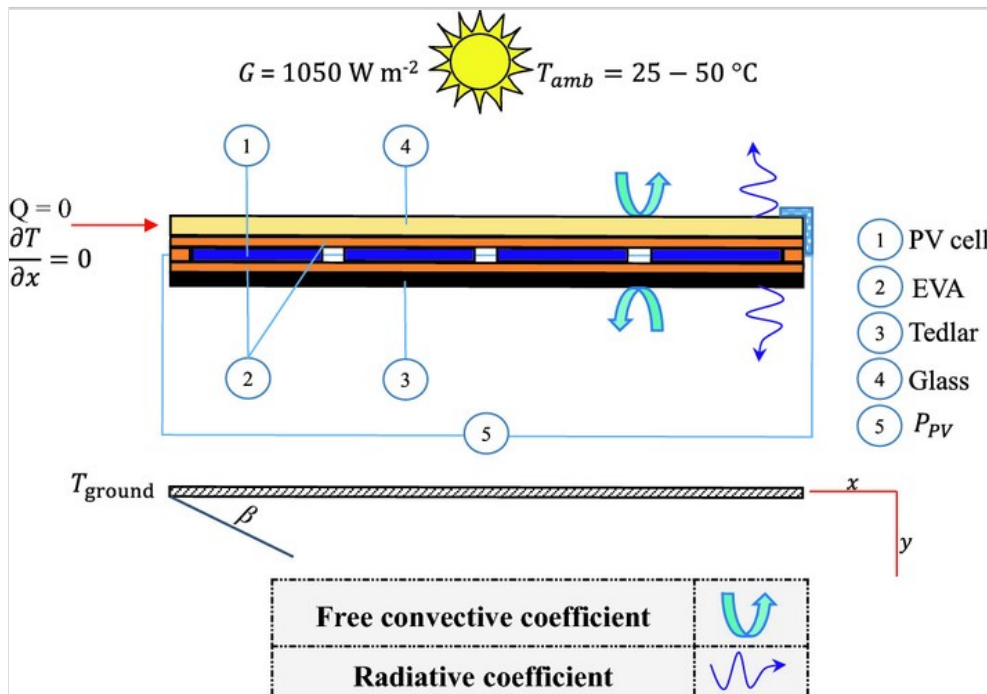
**Fig. 1**

Schematics of the PV/T air collector: in (a) 3D of single-duct single-pass (b) 2D cross-sectional front view and (c) 2D cross-sectional side view (not to scale)



**Fig. 2**

Description of the main heat transfer modes and components of standard PV module



**Table 1**

Dimension of PV/T air collectors in m

Collector length $L$ (m)	1.332
Collector width $w$ (m)	0.666
Duct depth $\delta_D$ (m)	0.025
Bottom absorber plate thickness (m)	0.001

Absorber plate thickness (m)	0.001
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**Table 2**

Physical properties of the PV module layers BP 585 [17].\*

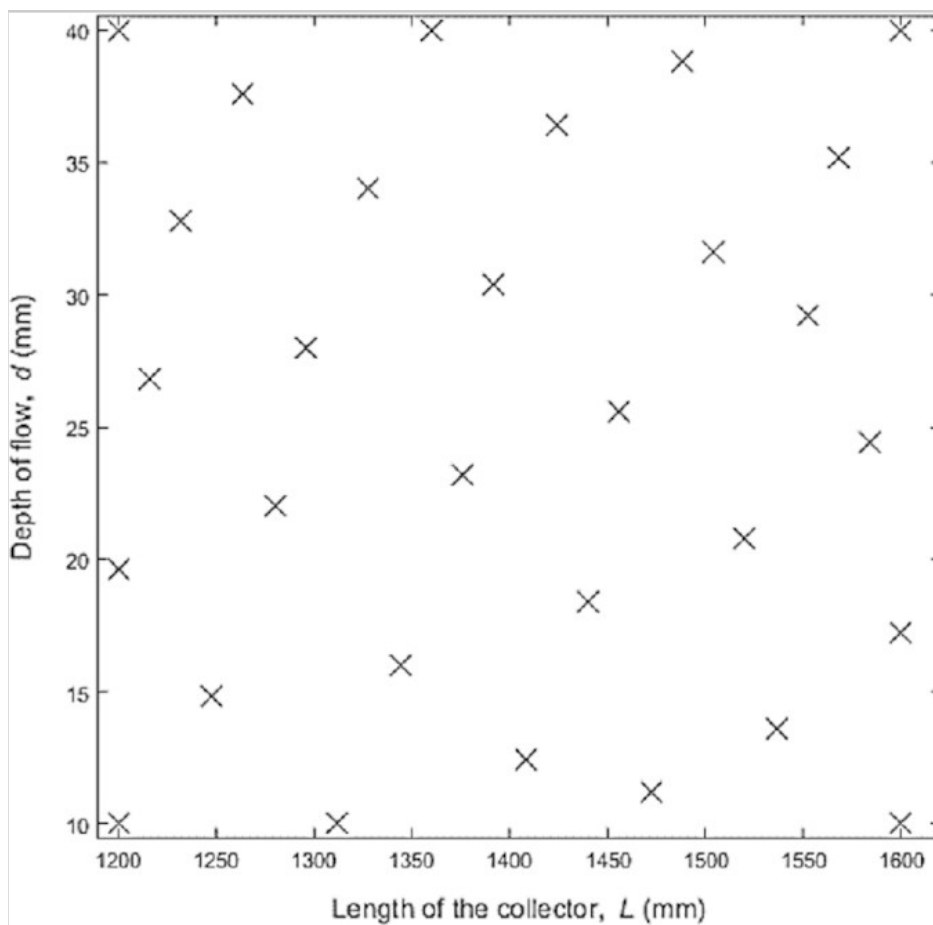
Layer	$t$ (mm)	$k$ (W m <sup>-1</sup> K <sup>-1</sup> )	$\rho$ (kg m <sup>-3</sup> )	$c$ (J kg <sup>-1</sup> C <sup>-1</sup> )	$\epsilon$
PV glass	3	1.8	3000	500	0.84
EVA	0.5	0.35	960	2090	–
PV cells	0.3	148	2330	677	0.7
Tedlar	0.5	0.2	1200	1250	0.87

\* $t$  is the thickness of PV module layers,  $k$  is the thermal conductivity of PV module layers,  $\rho$  is the density of PV module layers,  $c$  is the specific heat capacity of PV module layers, and  $\epsilon$  is the emmissivity of PV module layers

The governing equations for the air velocity  $\vec{V}(x, y, z) = u, v, w$  and temperature  $T$  are based on the conservations of mass, momentum, and energy inferred from [18, 19]. A CFD-based optimization analysis is carried out to minimize both pressure drop and thermal resistance as a function of two design variables: the length of the collector ( $L$ ) and the depth of the flow ( $\delta_D$ ). The design of experiment is constructed with 30 points in the two dimensions corresponding to their respective design variable ranges of 1.2 m  $\leq L \leq$  1.6 m and 0.01 m  $\leq \delta_D \leq$  0.04 m. The uniform distribution of the DoE points is shown in Fig. 3. The resulting Pareto front emphasizing to comprise that needs to be met to minimize both pressure drop and thermal resistance will be laid out.

**Fig. 3**

Design of experiments of single-duct signal-pass PV/T air collector



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### 3. Results

Numerical investigations were performed using COMSOL Multiphysics V5.3a to assess the influence of the PV panel temperature on the monocrystalline PV. To ensure the accuracy of the results, two validations with an experimental

set-up were conducted by Amori and Abd-AlRaheem [20] and Amori and Al-Najjar [21], and a good agreement was obtained. The first validation between current PV/T model and Amori and Abd-AlRaheem [20] is given in Table 3. The second validation between PV module (subject to ambient conditions), Amori and Abd-AlRaheem [20], and current CFD model is depicted in Fig. 4.

**Table 3**

Comparison between CFD model and measurement of [20]

Type	Ref. [20]	CFD
$T_g$	79.49	80.7
$T_{pv}$	81.22	80.1
$T_{Tedlar}$	74.51	79.63
$T_{fm}$	53.64	48.62
$T_{fo}$	61.51	52.1

**Fig. 4**

Validation between experimental and current CFD models for standard PV module subject to ambient conditions

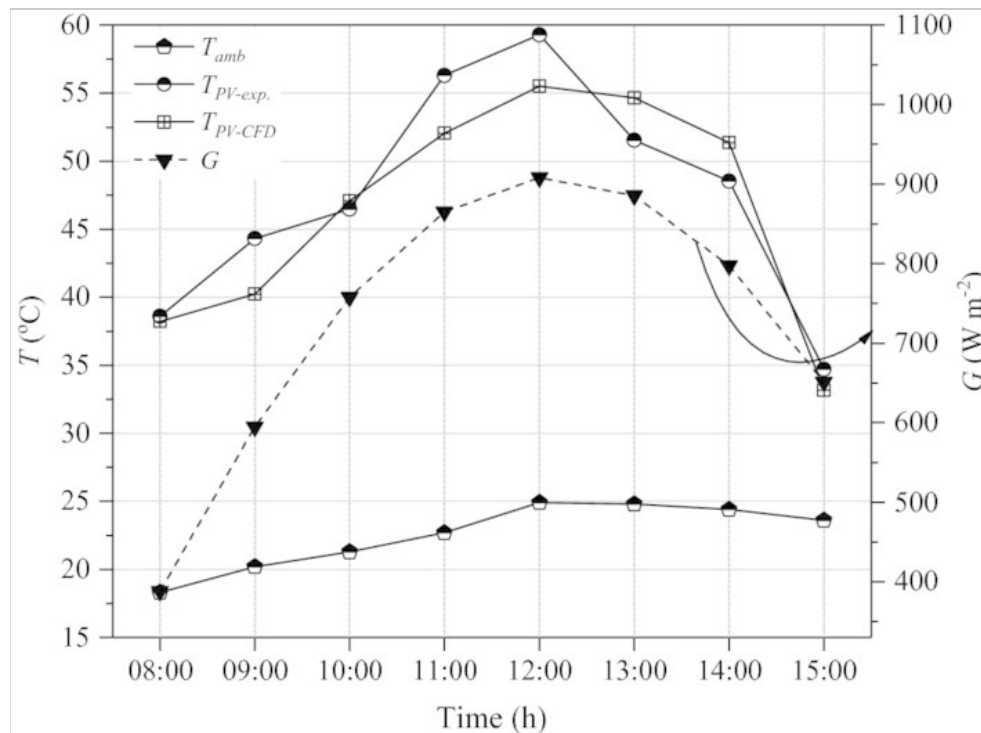
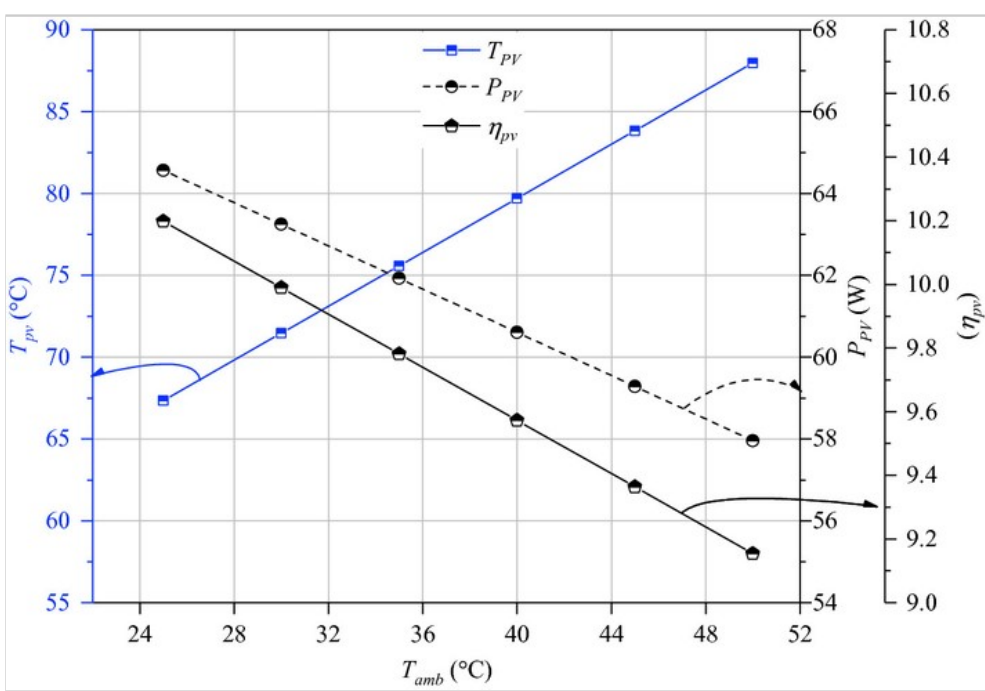


Figure 5 presents the effect of PV temperature on the PV output power under different ambient conditions for standard PV module without active cooling. Predictably, the PV power decreases with increasing PV module temperature. Figure 6 shows the influence of PV temperature on the PV output power under different ambient conditions for PV/T air system. The PV power also decreases with increasing PV module temperature. Figure 7 also reveals the influence of the PV and ambient temperatures (inlet fluid temperatures) on the thermal, electrical, and combined efficiency. It is apparent from this figure that electrical efficiency decreases with increasing PV panel temperature; however, the thermal and combined efficiency increases. Figure 8 presents the temperature gradient across the PV module. It can be seen that the PV cell has the maximum temperature since the electrical power generated in this domain. Figure 9 presents the temperature gradient along the PV/T collector. The temperature in the inlet region is low compared to the rest of the length as this region represents the non-fully developing region, which has a higher heat transfer coefficient. A comparison was made between PV and PV/T air system performances for weather conditions:  $G = 1050 W m^{-2}$ ,  $T_{amb} 25-50 ^\circ C$ , and  $Re = 2300$ , as shown in Fig. 10. The resultant data shows that PV power generation for PV/T air system is better than PV without active cooling even at higher temperature ( $50 ^\circ C$ ), since the PV panel temperature is lower for PV/T air collector.

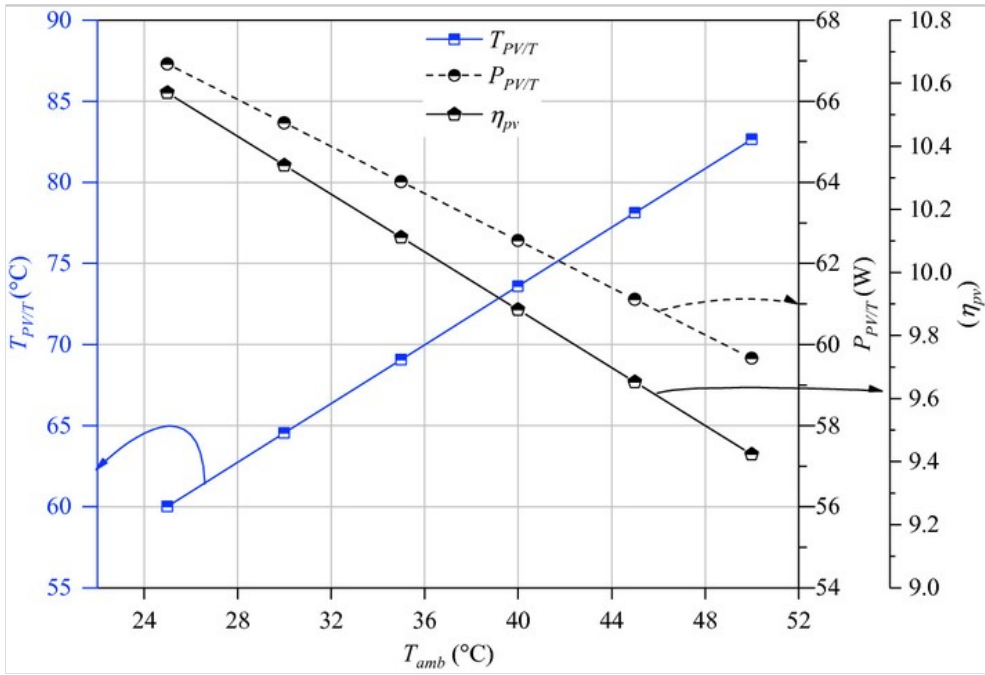
**Fig. 5**

Effect of different ambient temperatures under same insolation on power of standard PV module



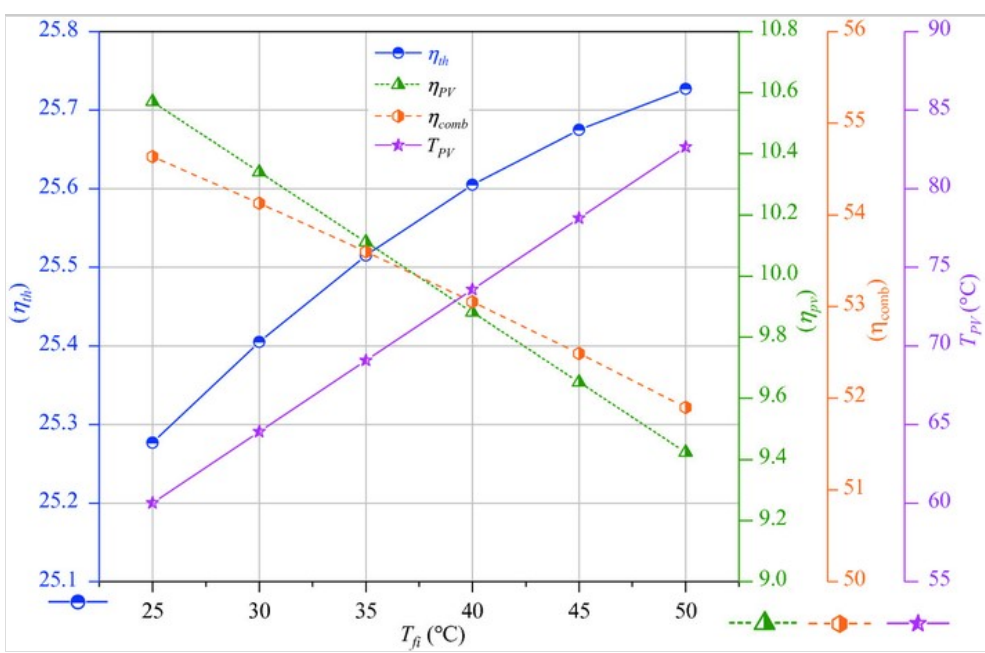
**Fig. 6**

Effect of different ambient temperatures under same insolation on power of PV/T air system



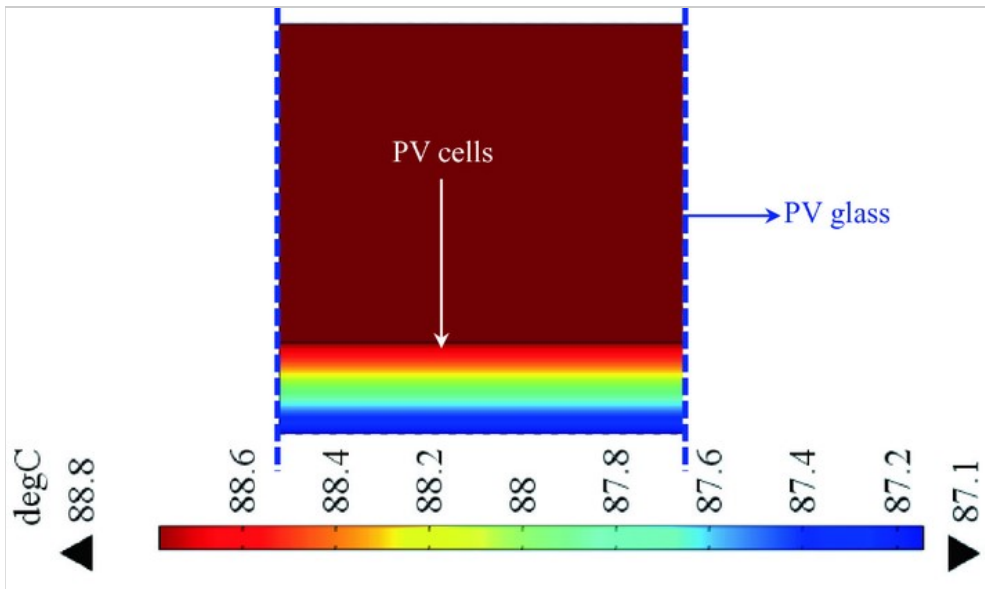
**Fig. 7**

Influence of PV temperature and inlet fluid temperature on thermal, electrical, and combined efficiency



**Fig. 8**

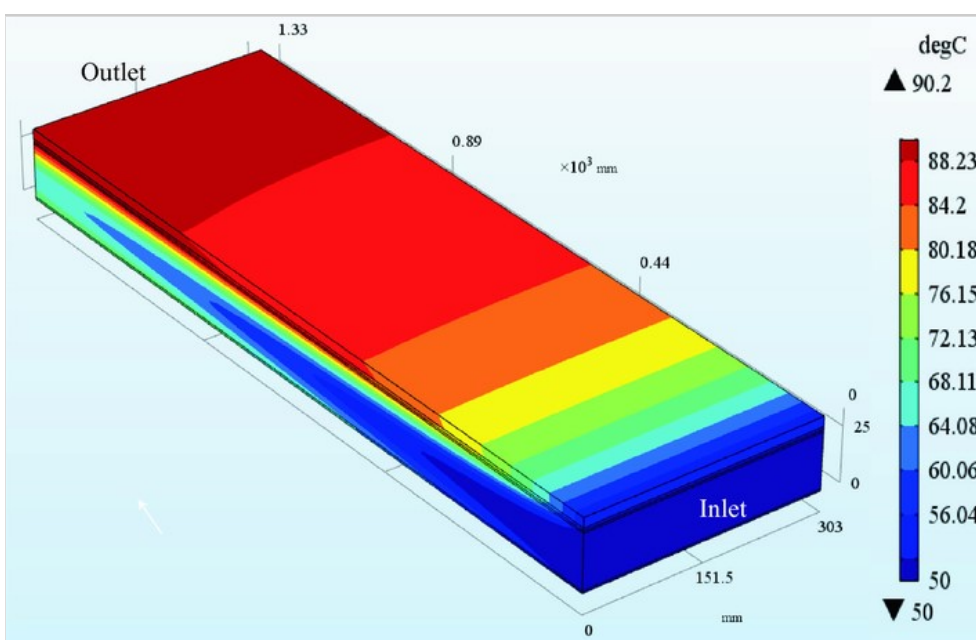
Temperature surface gradient of standard PV module (section side view) at the ambient conditions of  $T_{amb} = 50$  °C,  $Re = 2300$ ,  $G = 1050$  W.m<sup>-2</sup>



**Fig. 9**

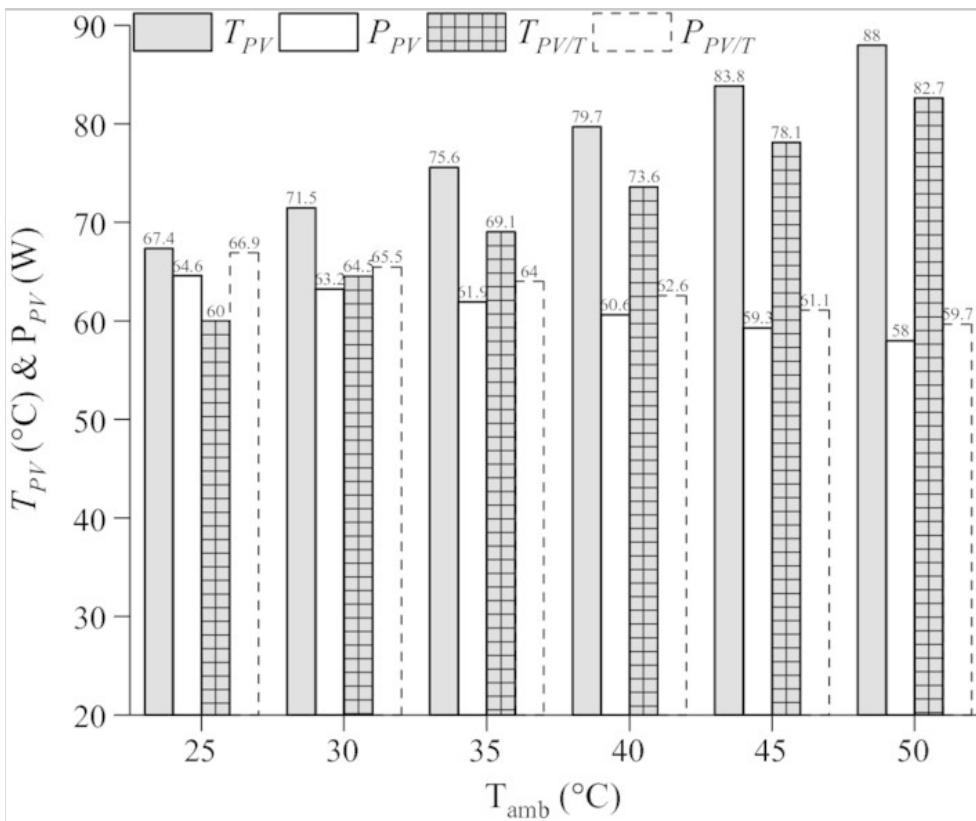
Temperature surface gradient of isometric 3D view of the PV/T system, for the same ambient conditions as Fig. 8





**Fig. 10**

Comparison between PV and PV/T air system performances for ambient temperature range  $T_{amb} = 25\text{--}50\text{ }^{\circ}\text{C}$ , and the same other conditions as those of Figs. 8 and 9



## 4. Conclusion

Based on the findings, the cooling system can be developed to provide higher performance PV systems. Under the worst-case scenario ( $1050\text{ W m}^{-2}$  and  $50\text{ }^{\circ}\text{C}$ ) and lower fan consumption (laminar flow condition  $Re = 2300$ ). The air cooling system is effective in reducing the PV temperature (increase PV efficiency). In addition, the overall collector efficiency increases. Future work will focus on using a novel heat sink design in cooling PV systems, with optimization of the collector dimensions and employing a different channel or flow type. The numerical investigation was conducted to evaluate the performance of two PV thermal designs. The first design was a PV module without active cooling (subjected to the ambient conditions) while the second design was a single duct single pass PV/T design with active cooling. The two systems were evaluated under the same conditions (under the worst-case scenario ( $1050\text{ W m}^{-2}$  and  $50\text{ }^{\circ}\text{C}$ ) and lower fan consumption (laminar flow condition  $Re=2300$ ). Based on the findings, the PV/T design can provide higher performance than the PV system. The air cooling system is effective in reducing the PV temperature (increase PV efficiency). Besides, the overall collector efficiency increases.

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